

UNIVERSITÀ DI PISA

FINTE ELEMENT MODEL OF HUMAN FINGERTIP

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Abstract

The fingertip deformation represents the basic mechanical action that shapes human haptic perception. Everyday, humans use their fingertips (and hands) to explore, manipulate and grasp the external environment for many tasks, ranging from simple object grasping towards complex palpation procedures used for medical diagnoses. Moreover, the investigation of fingertip sensing and mechanical properties has gained an increasing attention not only for modeling human behavior, but also in humanoid robotics, where the need for compliant robotic fingers endowed with tactile sensors has become crucial. In this work, we present an experimental set up to provide a characterization of human fingertip mechanical properties, in terms of contact area, fingertip deformation and pressure distribution. Such measures, obtained from experimental tests, are then correlated with the output of a 3D Finite Element (FE) Model of fingertip developed in order to validate the proposed study.

Experimental Tests

Numerical Model





Fig.1 Virtual test-rig

Fig.2 Physical test-rig

- The **displacement** is given by a linear DC actuator with 9.2 N of full scale.
- The forces and torques are recorded using a 6-DoF force/torque sensor (ATI 6-DoF Nano17).
- The contact area is acquired visually using a video camera, with 1500 x 1120.
- Subject placed the finger pad on the fingerholder, and the indenter surface was moved toward the finger pad.
- The finger was fixed to the finger-holder on







 Tab.2 Linear-elatic mechanical properties

the top of the nail, and it was oriented at a 15 deg angle [1].

Displacement of indentation 3 mm Velocity of indentation 1 mm/s



Fig.4 Experimental test

The subcutaneous tissue was present an hyperelastic behavior and it was modelled by using a Mooney-Rivlin model [2].

✤ 31672 elements and 77829 DOF.

In order to optimize the simulation time, the finger model was divided in two parts according to the sagittal symmetrical plane.

Parameters	C ₁₀	<i>C</i> ₀₁	<i>C</i> ₂₀	<i>C</i> ₁₁	<i>C₀₂</i>	D_1
ubcutaneous T.	300	671	29800	32700	9330	106.5

 Tab.3 Hyperelastic mechanical properties

A: Transient Structura

A Plate Displacemer

Nall Fixed

Time: 3, s

Mooney-Rivlin formulation

 $W = C_{10}(\bar{I}_1 - 3) + C_{01}(\bar{I}_2 - 3) + C_{20}(\bar{I}_1 - 3)^2 + C_{11}(\bar{I}_1 - 3)(\bar{I}_2 - 3)$

 $+ C_{02} (I_2 - 3)^2 + 1/d (J - 1)^2$

 $C_{10}, C_{01}, C_{20}, C_{11}, C_{02}$ d = material constants



Fig.7 Symmetric plane

✤ All contacts were modeled



CONTACT AREA: the one between the finger and the plate (blue one in Fig.10)

PRESSURE AREA: the one corresponding to the maximum value of pressure [Pa] (red one in Fig. 10) [1].



Fig.10 *Numerical results*

3. Comparison and Validation

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Experimental and Nume Contact A	rical Values Comparison rea [mm²]	Experimental and Numerical Values Comparison Force [N]		
Experimental Contact Area	133 ± 16.8	Experimental Force	1.71 ± 0.06	
Numerical Contact Area	129	Numerical Force	1.90	
Accuracy [%]	12.1	Accuracy [%]	11.1	

Tab.3 Comparison between Experimental and Numerical Values in terms of Contact Area and Force

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as **bonded contacts**, except contact between the the finger and the plate which was modeled as a **frictionless** contact.

* A fixed support constraint was applied on the nail and a displacement of 0.1 mm/s over 30 seconds (3 mm overall) was imposed to the lower face of the plate.



[1] Maria Laura D'Angelo, F. Cannella, M. Memeo, M.D'Imperio and M. Bianchi . "Preliminary Fingertip Pressure Area Distribution Via Experimental Test and Numerical Model" (2015 XXI IMEKO World Congress) [2] Gerling, G.J.; Rivest, I.I.; Lesniak, D.R.; Scanlon, J.R.; Lingtian Wan. "Validating a Population Model of Tactile Mechanotransduction of Slowly Adapting Type I Afferents at Levels of Skin Mechanics, Single-Unit Response and Psychophysics," IEEE Transactions on haptics.

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